# DETERMINATION OF THE INITIAL DATA FOR TRIANGULATION NET WITHOUT BASE-LINE 

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## ABSTRACT


#### Abstract

The present study gives a simplified solution to determine the initial data (base-line length and azimuth) for triangulation nets of low-order connected to a higher-order triangulation net. This may be achieved through the knowledge of the coordinates of two far-apart stations included in the lowerorder triangulation net. The author gives a mathematical treatment for determining all the elements of the initial data in this case, and accordingly, the triangulation adjustment may be performed. A sample numerical example is also presented according to the suggested formulas.


## 1. INTRODUCTION

A triangulation system basically consists of a configuration of triangles all of whose angles have ben directly measured. Sides whose lengths are rctually measured are known as basis or baseline. The survey points or triangulation stations are loated at the vertices of the triangles. By the use of the measured angles and bases, the lengths of all other sides in a connected system can be successively determined by trigonometry.
A cardinal principle in the extension of horizontal control is that of initially establishing master frameworks of reference, such as networks of highorder triangulation and subsequently subdividing such networks into secondary and tertiary systems of successively lower quality. This principle is sometimes termed "working from the whole to the part" [4].
In some practical cases to adjust a low-order triangulation network connected with a higher-order net, the initial data required may be missing and unknown due to various reasons.
In accordance, the present study aims to give a simplified procedure to obtain the initial data required for the adjustment of a secondary triangulation scheme. This procedure involves a mathematical treatment where the known coordinates of two stations of the network are used. These two stations do not represent the end-points of a base-line, but rather, are located in the triangulation net far apart from each other.

## 2. METHOD OF ANALYSIS

In a narrow triangulation system a chain of figures is employed, consisting of two triangles and a central-point figure (Figure (1)).


Figure 1.


Figure 2.
From (Figure (1)) the chain of single triangles shown in (Figure (2)) is chosen; there is but one
route by which distances can be computed through the chain. Also points M and N are fixed, and the coordinate-differences between them are $\Delta X_{M N}$, $\Delta \mathrm{Y}_{\mathrm{MN}}$. All the angles of the triangles are denoted $\mathrm{A}_{\mathrm{i}}$, $\mathrm{B}_{\mathrm{i}}$ and $\mathrm{C}_{\mathrm{i}}$.
From the length of the triangle sides $\mathrm{Ma}, 1,2,3,4,5$ and through the route $\mathrm{Ma}-\mathrm{ab}-\mathrm{bc}-\mathrm{cd}-\mathrm{de}-\mathrm{eN}$ in the chain (Figure (2)), the difference in coordinates between points M and N may be obtained from the following equation [3]:

$$
\left.\begin{array}{l}
\Delta X_{M N}=S_{M a} \cos \alpha_{M a}+S_{1} \cos \alpha_{1}+\ldots+S_{\mathrm{n}} \cos \alpha_{\mathrm{n}}  \tag{1}\\
\Delta \mathrm{Y}_{\mathrm{MN}}=\mathrm{S}_{\mathrm{Ma}} \sin \alpha_{\mathrm{Ma}}+\mathrm{S}_{1} \sin \alpha_{1}+\ldots+\mathrm{S}_{\mathrm{n}} \sin \alpha_{\mathrm{n}}
\end{array}\right\}
$$

where: $\mathrm{S}_{\mathrm{Ma}}, \alpha_{\mathrm{Ma}}$ are the length and azimuth of side Ma , and $\mathrm{S}_{\mathrm{i}}, \alpha_{\mathrm{i}}$ are the length and azimuth of side " i ".
To obtain the elements $\mathrm{S}_{\mathrm{Ma}}$ and $\alpha_{\mathrm{Ma}}$, the following procedure is made [1]

$$
\begin{equation*}
S_{i}=S_{M a} \frac{\sin A_{1} \sin A_{2} \ldots \cdot \sin A_{i}}{\sin \beta_{1} \sin \beta_{2} \ldots \cdot \sin \beta_{i}} \tag{2}
\end{equation*}
$$

and

$$
\begin{equation*}
\alpha_{i}=\alpha_{M a}+\sum_{j=1}^{i}\left[(-1)^{j} C_{j}+180^{\circ}\right] \tag{3}
\end{equation*}
$$

If we consider that:

$$
\begin{gather*}
K_{1}=\frac{\sin A_{1}}{\sin \beta_{1}}, \quad k_{i}=\frac{\sin A_{1} \ldots \sin A_{i}}{\sin \beta_{1} \ldots \cdot \sin \beta_{i}}  \tag{4}\\
Z_{i}=\sum_{j=1}^{i}(-1)^{j+1} C_{j},  \tag{5}\\
K_{i}=K_{i-1} \frac{\sin A_{i}}{\sin \beta_{i}}, \quad\left(k_{o}=1\right) \tag{6}
\end{gather*}
$$

Formulas (2) and (3) may therefore be re-written in the following form: [1]

$$
\begin{gather*}
S_{i}=S_{M a} K_{i}  \tag{7}\\
\alpha_{i}=\left(\alpha_{M a}-Z_{i}\right)+180^{\circ} . i \tag{8}
\end{gather*}
$$

After simple conversion, formula (1) can be finally expressed in the form:

$$
\begin{align*}
\Delta X_{M N}= & \Delta X_{M a}\left[1-K_{1} \cos Z_{1}+\ldots+(-1)^{n} K_{n} \cos Z_{n}\right]+ \\
& +\Delta Y_{M a}\left[-K_{1} \sin Z_{1}+\ldots+(-1)^{n} K_{n} \sin Z_{n}\right]  \tag{9}\\
\Delta Y_{M N}= & \Delta Y_{M a}\left[1-K_{1} \cos Z_{1}+\ldots+(-1)^{n} K_{n} \cos Z_{n}\right]- \\
& -\Delta X_{M a}\left[-K_{1} \sin Z_{1}+\ldots+(-1)^{n} K_{n} \sin Z_{n}\right]
\end{align*}
$$

To simplify the form of equation (9), consider that:

$$
\left.\begin{array}{l}
\epsilon_{i}=(-1)^{i} K_{i} \cdot \cos Z_{i}  \tag{10}\\
\eta_{i}=(-1)^{i} K_{i} \cdot \sin Z_{i}
\end{array}\right\}
$$

also, for further simplification,

$$
\left.\begin{array}{l}
E=1+\sum_{i=1}^{n} \epsilon_{i},  \tag{11}\\
H=\sum_{i=1}^{n} \eta_{i}
\end{array}\right\}
$$

Accordingly, formula (9) will have the form:

$$
\left.\begin{array}{c}
\Delta X_{\mathrm{MN}}=E \Delta X_{\mathrm{Ma}}+\mathrm{H} \Delta \mathrm{Y}_{\mathrm{Ma}}  \tag{12}\\
\Delta \mathrm{Y}_{\mathrm{MN}}=-\mathrm{H} \Delta \mathrm{X}_{\mathrm{Ma}}+\mathrm{E} \Delta \mathrm{Y}_{\mathrm{Ma}}
\end{array}\right\}
$$

Through equation (12) the components of side Ma are determined [2]:

$$
\begin{align*}
& \Delta X_{M a}=\frac{E \Delta X_{M N}-H \Delta Y_{M N}}{E^{2}+H^{2}}  \tag{13}\\
& \Delta Y_{M a}=\frac{E \Delta Y_{M N}+H \Delta X_{M N}}{E^{2}+H^{2}}
\end{align*}
$$

Thus, the values of $\mathrm{S}_{\mathrm{Ma}}, \alpha_{\mathrm{Ma}}$ for triangle I (Figure (2)) are given by:

$$
\begin{gather*}
S_{\mathrm{Ma}}=\sqrt{\frac{\Delta \overline{\mathrm{X}}_{\mathrm{MN}}^{2}+\Delta \overline{\mathrm{Y}}_{\mathrm{MN}}^{2}}{\mathrm{E}^{2}+\mathrm{H}^{2}}}=\sqrt{\frac{\mathrm{S}_{\mathrm{MN}}^{2}}{\mathrm{E}^{2}+\mathrm{H}^{2}}}  \tag{14}\\
\alpha_{\mathrm{Ma}}=\arctan \frac{\Delta \mathrm{Y}_{\mathrm{Ma}}}{\Delta \mathrm{X}_{\mathrm{Ma}}} \tag{15}
\end{gather*}
$$

## 3. DETERMINATION OF PROVISIONAL COORDINATES

The components of the sides of the chain are obtained from:

$$
\left.\begin{array}{l}
\Delta X_{i}=\epsilon_{i} \Delta X_{\mathrm{Ma}}+\eta_{i} \Delta Y_{M a}  \tag{16}\\
\Delta Y_{i}=\epsilon_{\mathrm{i}} \Delta Y_{\mathrm{Ma}}-\eta_{\mathrm{i}} \Delta \mathrm{X}_{\mathrm{Ma}}
\end{array}\right\}
$$

The provisional coordinates of the chain may be obtained by using the above components.
From the previous, the final adjusted coordinates may be obtained by applying a rigorous least squares method of adjustment.

## 4. A SAMPLE NUMERICAL EXAMPLE

Figure (2) illustrates a chain of adjoined triangles between two fixed stations M and N . All the angle of the triangles are observed [3]. The coordinates of the fixed stations M and N are: $(20500.1,20500.2)$, $(1521.9,41792.8)$ respectively. The solution procedure and results are tabulated in tables (1) and (2).
$\Delta \mathrm{X}_{\mathrm{MN}}=-18978.20, \Delta \mathrm{Y}_{\mathrm{MN}}=+21292.60$
From equation (13)
$\Delta \mathrm{X}_{\mathrm{Ma}}=+5586.36, \Delta \mathrm{Y}_{\mathrm{Ma}}=+14021.27$
Also, from equations (14) and (15):
$\mathrm{S}_{\mathrm{Ma}}=15093.16 \mathrm{M}, \alpha_{\mathrm{Ma}}=68^{\circ} 16^{\prime} 34.1^{\prime \prime}$.

Table 1. Calculation of values $Z$ and $K$..

| No. of <br> triangle | No. of <br> angle | Observed <br> angles | Corr. | Adjusted <br> angles | $\sin \mathrm{A}_{\mathrm{i}}$, $\sin \beta_{\mathrm{i}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | $22^{\circ} 19^{\prime} 50^{\prime}$ | $-2^{\prime \prime}$ | $22^{\circ} 19^{\prime} 48^{\prime \prime}$ | 0.379941 |
| I | 2 | 1222245 | -1 | 1201944 | 0.862675 |
|  | 3 | 371730 | -2 | 371728 |  |
|  |  | $\omega=+5^{\prime \prime}$ | $-5^{\prime \prime}$ | $\mathrm{Z}_{1}=37^{\circ} 17^{\prime} 28^{\prime \prime}$ | $\mathrm{k}_{1}=0.440422$ |
|  | 4 | 545920 | -3 | 545917 | 0.819037 |
| II | 5 | 492150 | -3 | 492147 | 0.758851 |
|  | 6 | 753900 | -4 | 753956 |  |
|  |  | $\omega=+10^{\prime \prime}$ | -10 | $\mathrm{Z}_{2}=-38^{\circ} 21^{\prime} 28^{\prime \prime}$ | $\mathrm{k}_{2}=0.475353$ |
|  | 7 III | 8 | 473710 | +2 | 473712 |
|  | 394525 | +2 | 394527 | 0.738691 |  |
|  | 9 | 923720 | +1 | 923721 | 0.639577 |
|  |  | $\omega=-5^{\prime \prime}$ | $+5^{\prime \prime}$ | $\mathrm{Z}_{3}=54^{\circ} 15^{\prime} 53^{\prime \prime}$ | $\mathrm{k}_{3}=0.549018$ |
| IV | 10 | 374735 | 0 | 374635 | 0.612581 |
|  | 11 | 840740 | 0 | 840740 | 0.994753 |
|  | 12 | 580545 | 0 | 580545 | - |
|  |  | $\omega=0.0^{\prime \prime}$ | 0 | $Z_{4}=3^{\circ} 49^{\prime} 52^{\prime \prime}$ | $\mathrm{k}_{4}=0.338092$ |
| V | 13 | 471810 | +3 | 741813 | 0.962709 |
|  | 14 | 281350 | +4 | 281354 | 0.473038 |
|  | 15 | 772750 | +3 | 772753 | - |
|  |  | $\omega=-10^{\prime \prime}$ | $+10^{\prime \prime}$ | $Z_{5}=73^{\circ} 38^{\prime} 01^{\prime \prime}$ | $\mathrm{k}_{5}=0.688072$ |

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Table 2. Calculation of values $\epsilon, \eta, \mathrm{E}, \mathrm{H}, \Delta \mathrm{X}_{\mathrm{i}}$ and $\Delta \mathrm{Y}_{\mathrm{i}}$.

| No of sides | $\bar{Z}$ $\cos Z$ <br> $\operatorname{Sin} Z$ | $(-1)^{i} \mathrm{~K}_{\mathrm{i}}$ | $\epsilon$ | $\therefore \quad \eta$ | $\begin{gathered} \epsilon_{\mathrm{i}} \Delta \mathrm{X}_{\mathrm{Ma}} \\ +\eta_{\mathrm{i}} \Delta \mathrm{Y}_{\mathrm{Ma}} \\ \frac{\Delta \mathrm{X}_{\mathrm{i}}}{} \end{gathered}$ | $\begin{gathered} \epsilon_{\mathrm{i}} \Delta \mathrm{Y}_{\mathrm{Ma}} \\ - \\ \eta_{\mathrm{i}} \Delta \mathrm{X}_{\mathrm{Ma}} \\ \frac{\Delta \mathrm{Y}_{\mathrm{i}}}{} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M-a | - | 1 | 1 | 0 | +55866.36 | +14021.27 |
| 1 | $\begin{gathered} 37^{\circ} 17^{\prime} 28^{\prime \prime} \\ 0.795568 \\ 0.605864 \end{gathered}$ | -0.440422 | -0.350386 | -0.266883 | $\begin{aligned} & -1957.38 \\ & -3741.38 \\ & \hline-5698.76 \end{aligned}$ | $\begin{aligned} & -4912.86 \\ & -1490.64 \\ & \hline-3422.22 \end{aligned}$ |
| 2 | $\begin{gathered} -38^{\circ} 21^{\prime} 28^{\prime \prime} \\ 0.784137 \\ -0.62057 \end{gathered}$ | +0.475353 | +0.372742 | -0.294999 | $\begin{aligned} & \hline+2082.77 \\ & -4136.14 \\ & -2053.87 \end{aligned}$ | $\begin{aligned} & +5226.32 \\ & -1647.92 \\ & +6874.24 \end{aligned}$ |
| 3 | $\begin{gathered} 54^{\circ} 15^{\prime} 53^{\prime \prime} \\ 0.584041 \\ 0.811724 \end{gathered}$ | -0.549018 | -0.320649 | -0.44565 | $\begin{array}{r} -1791.26 \\ -6248.59 \\ \hline-8039.85 \end{array}$ | $\begin{array}{r} -4495.91 \\ -2489.57 \\ \hline-2006.34 \end{array}$ |
| 4 | $\begin{gathered} -3^{\circ} 49^{\prime} 52^{\prime \prime} \\ 0.997766 \\ -0.066816 \end{gathered}$ | +0.338092 | +0.338092 | -0.022590 | $\begin{gathered} +1884.48 \\ \underline{-316.74} \\ +1567.74 \end{gathered}$ | $\begin{gathered} +4729.89 \\ +-126.20 \\ +4856.09 \end{gathered}$ |
| 5 | $\begin{gathered} 73^{\circ} 38^{\prime} 01^{\prime \prime} \\ 0.281778 \\ 0.959479 \end{gathered}$ | -0.688072 | -0.193884 | -0.660190 | $\begin{array}{r} -1083.10 \\ -9256.72 \\ \hline-10339.82 \end{array}$ | $\begin{aligned} & -2718.50 \\ & -3688.06 \\ & \hline+969.56 \end{aligned}$ |
|  |  |  | $\mathrm{E}=0.845160$ | $\mathrm{H}=-1.690258$ |  |  |

Therefore, $\mathrm{E}^{2}+\mathrm{H}^{2}=3.571268$

## 5. CONCLUSIONS

The paper involves the presentation of a straightforward simplified procedure to determine the necessary initial data, base-line length and azimuth which may by missing and unknown, required for the adjustment of a triangulation net.
The verification of the procedure is illustrated by a numerical example.

## REFERENCES

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