

AN ALTERNATIVE METHOD FOR CALCULATING THE RESPONSE OF CARDIAC TISSUE TO STIMULATING CURRENTS

A.M. KHALIFA, Ph.D.

**Dept. of Electrical Engineering Alex., University
Alexandria, Egypt.**

ABSTRACT

Response of a one dimensional myocardial fiber to a constant stimulating current was analysed by R. Plonsey and R.C. Barr [1], [2]. An alternative simple method is presented in this communication to solve the problem. The fiber is regarded as cascaded sections. Results obtained are almost identical to those obtained from the exact method by R. Plonsey and R.C. Barr.

INTRODUCTION

The effect of a defibrillating stimulus current when applied to a one dimensional fiber with a junction resistance joining the individual cells was analysed by R.Plonsey & R.C. Barr [1], [2]. They have solved the problem by three methods, the first two are approximate and, the third one is exact. In the exact method they considered the solution to be a combination of two more easily solved problems.

- a) The primary source solution was obtained by setting the coupling resistance to zero. Thus the cells would constitute a single continuous fiber.
- b) The secondary source solution took into account the effect of junction resistance. This was obtained by considering the effect of each junction resistance as a dipole source placed at the junction. This method involves solution of 29 simultaneous equations and does not give the exact solution for the transmembrane potentials in a direct way. Therefore, in the present work a simple approach is proposed to give a direct solution for currents and voltages at the junction and at any point along each cell.

THEORETICAL ANALYSIS

The proposed method is based on representing the fiber as a

cascaded sections (Fig. 1). Each section represents one cell as a uniform T.L. with its junction resistance connected to its receiving end.

Considering the T.L. equations for one of the cells (Fig. 2) we get:

$$\frac{dV_m}{dX} = -i(x)(r_e + r_i) + I_o \cdot r_e \quad (1)$$

$$V_m(x) = -r_m \frac{di(x)}{dX} \quad (2)$$

where :

$V_m(x)$ = transmembrane voltage.

$i(x)$ = induced loop current.

I_o = injected current

r_m = transmembrane resistance per unit meter

r_i = intercellular resistance per unit meter

r_e = extracellular resistance per unit meter

Using equations (1) & (2)

$$\frac{d^2 V_m}{dX^2} = \frac{r_e + r_i}{r_m} \cdot V_m \quad (3)$$

The general solution for the above equation for cell number "k" is given by:

$$V_m = A_k \cdot \exp(\gamma x) + B_k \cdot \exp(-\gamma x) \quad (4-a)$$

$$i(x) = \frac{I_o \cdot r_e}{r_e + r_i} - \frac{\gamma}{r_e + r_i} (A_k \exp(\gamma x) - B_k \exp(-\gamma x)) \quad (4-b)$$

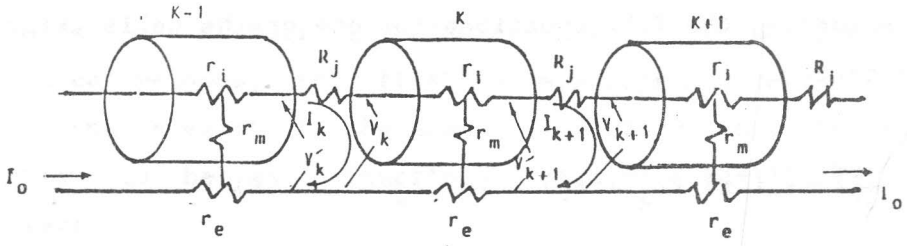


Fig. 1: Currents and voltages at the input and output of cell no. (k).

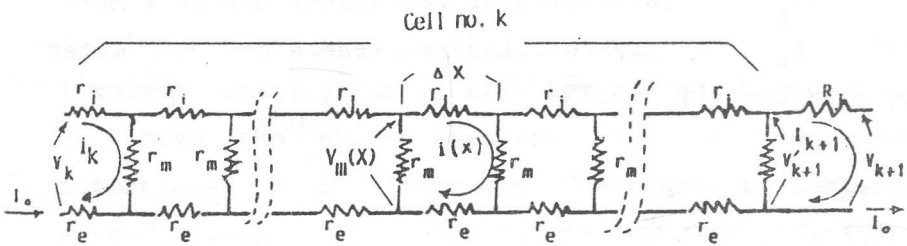


Fig. 2: Current and voltage distribution inside cell no. (K).

where , $\gamma = \sqrt{\frac{r_e + r_i}{r_m}}$

Applying the boundary conditions (Fig. 2) at $x = 0$

$V_m(x) = V_k$ and $i(x) = i_k$

and at $x = \ell$: (where ℓ is the cell length.)

$V_m(x) = V'_{k+1}$ and $i(x) = i'_{k+1}$

we get :

$A_k = 0.5 (V_k + Z_o. (I'_o - i_k))$ (5.a)

$B_k = 0.5 (V_k - Z_o. (I'_o - i_k))$ (5.b)

where,

$I'_o = I_o. \frac{r_e}{r_e + r_i}$ & $Z_o = \sqrt{r_m. (r_e + r_i)}$

From equations (4) & (5) we get :

$$\begin{bmatrix} V'_{k+1} \\ i'_{k+1} \\ I'_o \end{bmatrix} = \begin{bmatrix} A \\ B \end{bmatrix} \begin{bmatrix} V_k \\ i_k \\ I'_o \end{bmatrix} \quad (6)$$

where:

$$\begin{bmatrix} B \end{bmatrix} = \begin{bmatrix} \cosh \gamma l & -Z_0 \sinh \gamma l & Z_0 \sinh \gamma l \\ \frac{-\sinh \gamma l}{Z_0} & \cosh \gamma l & 1 - \cosh \gamma l \\ 0 & 0 & 1 \end{bmatrix}$$

and considering the effect of the junction resistance R_j (Fig.1) we get:

$$V_{k+1} = V'_{k+1} - R_j \cdot i_{k+1} \quad (7)$$

Using equations (6) & (7)

$$\begin{bmatrix} V_{k+1} \\ i_{k+1} \\ I'_0 \end{bmatrix} = \begin{bmatrix} G \end{bmatrix} \begin{bmatrix} V_k \\ i_k \\ I'_0 \end{bmatrix} \quad (8)$$

where:

$$\begin{bmatrix} G \end{bmatrix} = \begin{bmatrix} \cosh \gamma l + \frac{R_j}{Z_0} \sinh \gamma l & Z_0 \sinh \gamma l + R_j \cosh \gamma l & Z_0 \sinh \gamma l + R_j (1 - \cosh \gamma l) \\ \frac{-\sinh \gamma l}{Z_0} & \cosh \gamma l & 1 - \cosh \gamma l \\ 0 & 0 & 1 \end{bmatrix}$$

Using equations (6) & (8) and evaluating the cascade of 30 cells we get :

$$\begin{bmatrix} V_{31} \\ I_{31} \\ I'_0 \end{bmatrix} = \begin{bmatrix} G \end{bmatrix} \begin{bmatrix} B \end{bmatrix} \begin{bmatrix} V_1 \\ I_1 \\ I'_0 \end{bmatrix} \quad (9)$$

Using the boundary conditions, $I_1 = 0$ & $I_{31} = 0$, we get V_1 & V_{31} in terms of I_0 .

Starting with V_k , I_k and I_0 and using equation (8) we get V'_k , V_k & I_k for all cells. Using equation (5) and the values of V'_k , V_k & I_k , we get A_k & B_k for each cell and using equation (4) we get $V(x)$, $i(x)$ at any point inside each cell.

RESULTS AND DISCUSSION

Results obtained in this work are tabulated in tables (1) and (2). Table (1) shows almost identical values of cellular currents compared with those obtained by the exact method of Plonsey and Barr [1,2]. Table (2) shows the exact values of the transmembrane potentials V_m as obtained by the present work compared with those obtained by the approximate method of Poloney and Barr [1], [2]. The values of V_m obtained by their exact method are not published.

Membrane potential $V_m(x)$ along the cell is also obtained in this work (Equation 4):

The proposed method includes less calculation steps. Running the program in an IBM PC with double precision took less than 15 sec. This indicates less probable calculation error.

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| Node Number | a) $R_j=500 \text{ k}\Omega$ | | b) $R_j=849 \text{ k}\Omega$ | | $R_j=50 \text{ M}\Omega$ | |
|----------------|------------------------------|---------|------------------------------|---------|--------------------------|---------|
| | I_k | I_k^* | I_k | I_k^* | I_k | I_k^* |
| 1 | 582.83 | 583 | 554.57 | 555 | 115.16 | 115 |
| 2 | 1056.13 | 1056 | 1000.69 | 1001 | 168.26 | 168 |
| 3 | 1440.23 | 1440 | 1359.37 | 1359 | 192.75 | 193 |
| 4 | 1751.63 | 1752 | 1647.49 | 1647 | 204.04 | 204 |
| 5 | 2003.70 | 2004 | 1878.64 | 1979 | 209.24 | 209 |
| 6 | 2207.28 | 2207 | 2063.69 | 2064 | 211.64 | 212 |
| 7 | 2371.11 | 2371 | 2211.37 | 2211 | 212.75 | 213 |
| 8 | 2502.24 | 2502 | 2328.62 | 2329 | 213.26 | 213 |
| 9 | 2606.29 | 2606 | 2420.97 | 2421 | 213.50 | 213 |
| 10 | 2687.74 | 2688 | 2492.77 | 2493 | 213.61 | 214 |
| 11 | 2750.07 | 2750 | 2547.39 | 2547 | 213.66 | 214 |
| 12 | 2795.98 | 2796 | 2587.42 | 2587 | 213.68 | 214 |
| 13 | 2827.43 | 2827 | 2614.74 | 2615 | 213.69 | 214 |
| 14 | 2845.78 | 2846 | 2630.63 | 2631 | 213.69 | 214 |
| 15 | 2851.81 | 2852 | 2635.85 | 2636 | 213.70 | 214 |

Table 1: Node currents I_k calculated by the method described in this paper and the values I_k^* obtained by POLONSEY and BARR [2].

| Node number | a) $R_j=500 \text{ k}$ | | b) $R_j=849 \text{ k}$ | | $R_j=50 \text{ M}$ | |
|----------------|------------------------|-----------------|------------------------|-----------------|--------------------|-----------------|
| | V_k | V_k^* (appx.) | V_k | V_k^* (appx.) | V_k | V_k^* (appx.) |
| 1 | -223.47 | -- | -212.22 | -213 | -49.88 | -48.9 |
| 2 | -182.15 | -- | -171.86 | -172 | -37.4 | -36.8 |
| 3 | -148.48 | -- | -139.30 | -140 | -31.64 | -31.4 |
| 4 | -121.03 | -- | -113.01 | -113 | -28.98 | -28.9 |
| 5 | -98.60 | -- | -91.76 | -92.2 | -27.76 | -27.7 |
| 6 | -80.25 | -- | -74.55 | -74.9 | -27.2 | -27.2 |
| 7 | -65.17 | -- | -60.57 | -60.9 | -26.94 | -27.0 |
| 8 | -52.73 | -- | -49.15 | -49.4 | -26.82 | -26.9 |
| 9 | -42.38 | -- | -39.76 | -40.0 | -26.76 | -26.9 |
| 10 | -33.68 | -- | -31.95 | -32.1 | -26.73 | -26.8 |
| 11 | -26.27 | -- | -25.37 | -25.5 | -26.72 | -26.8 |
| 12 | -19.81 | -- | -19.7 | -19.8 | -26.72 | -26.8 |
| 13 | -14.04 | -- | -14.66 | -14.8 | -26.71 | -26.8 |
| 14 | -8.7 | -- | -10.04 | -10.1 | -26.71 | -26.8 |
| 15 | -3.56 | -- | -5.59 | -5.6 | -26.71 | -26.8 |

Table 2: The transmembrane potential at the (K th) node V_k obtained by the method described in this paper and the values V_k^* (appx.) obtained by the approximate method described by POLONSEY and BARR [2]. V_k^* (appx) in case of $R_j = 500 \text{ k}$ is not published

REFERENCES

- [1] R.Plonsey & R.C. Barr "Effect of Microscopic and macroscopic discontinuities on the response of cardiac tissue to defibrilating (stimulating) currents", Med. & Biol. Eng. & Comput., 1986, 24, 130-136.
- [2] R. Plonsey & R.C. Barr "Inclusion of junction elements in a linear cardiac model through secondary sources: - application to defibrillation", Med. & Biol. Eng. & Compu., 1986, 24, 137-144.

List of Symbols

- $V_m(x)$ = the transmembrane voltage
 $i(x)$ = the induced loop current
 I_o = the injected current
 r_m = the transmembrane resistance times length ($\Omega \cdot m$)
 r_i = the intracellular resistance per unit meter (Ω /m)
 r_e = the extracellular resistance per unit meter (Ω /m)
 R_j = the junction resistance between two cells
 ℓ = the cell length
 V_k = the value of $V_m(x)$ at $x = 0$ for cell no. k
 V'_{k+1} = the value of $V_m(x)$ at $x = \ell$ for cell no. k